



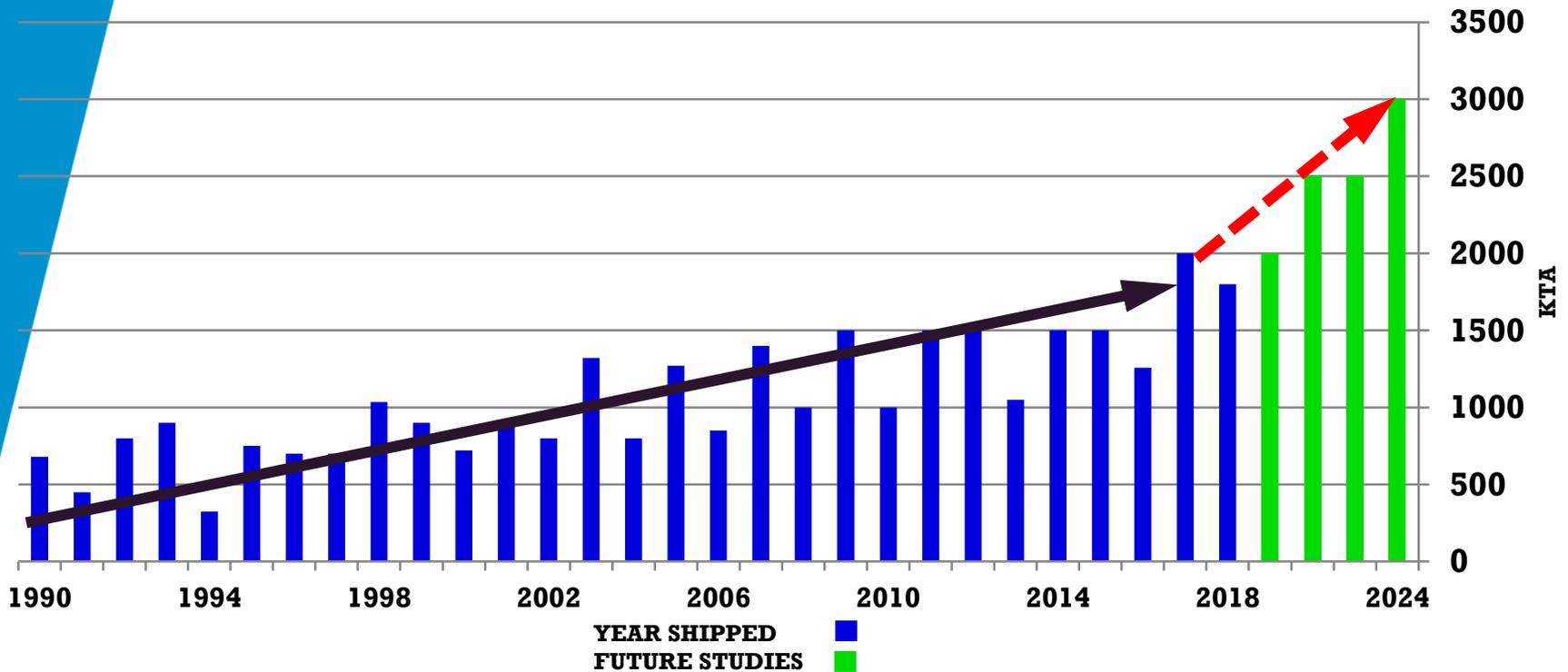
# Reducing Costs With the Application of High Flow Coefficient Impellers in the Main Compressors of Ethylene Plants

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# 1500KTA CGC String on Test



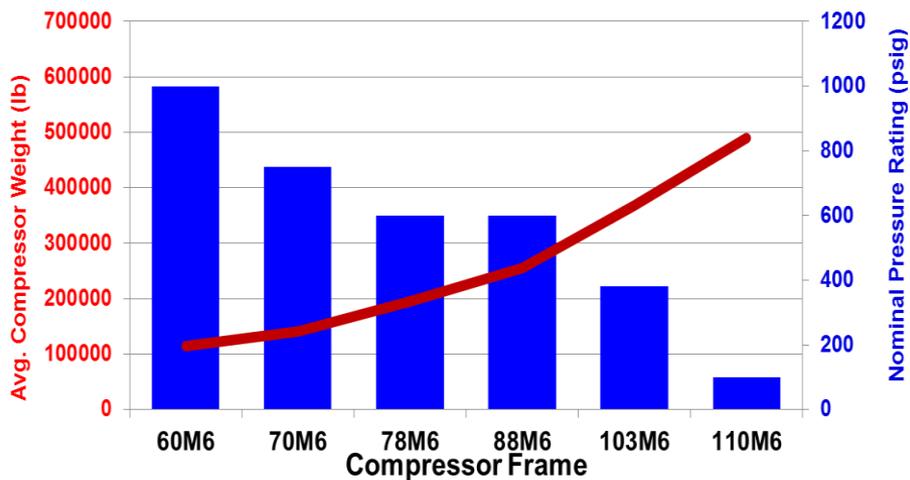
# Ethylene Capacity Trend



# The Problem:

If the industry continues to simply increase plant capacities and CGC inlet volume flows expecting to increase the scale of the compressors; economies of scale will disappear.

# Challenges of Larger Frames



# Solution:

Increase the flow capacity of the current frame size compressors.

- Adopting higher flow coefficient stages
- Applying larger nozzles onto the frame size
- Reducing stage spacing of existing stages

# Compressor Flow Coefficient

$$\Phi = \frac{700Q}{Nd^3}$$

$\Phi$  = Flow Coefficient

$Q$  = Flow in CFM [ft<sup>3</sup>/min]

$N$  = RPM [1/min]

$d$  = Impeller Diameter [ft]

*Flow Rate divided by Speed and Diameter<sup>3</sup>*

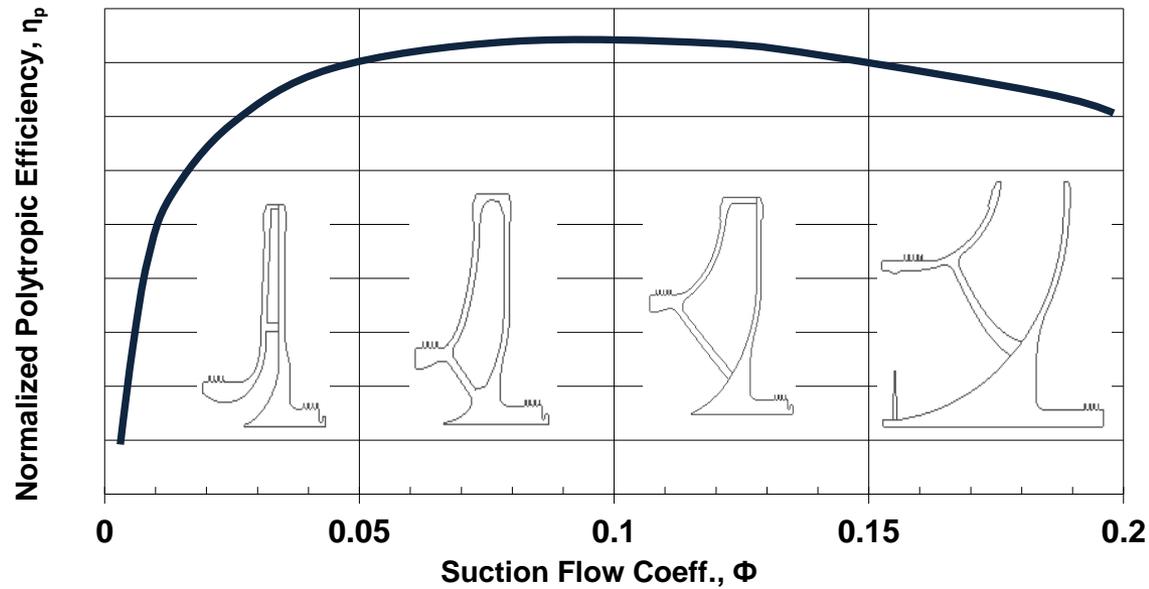
*Sometimes:*

$$\Phi = \frac{Q}{DU}$$

$\Phi$  = Flow Coefficient  $Q$  = Inlet Flow [m<sup>3</sup>/s]

$D$  = Impeller Diameter [m]  $U$  = Tip Speed [m/s]

# Radial Flow Centrifugal Stage



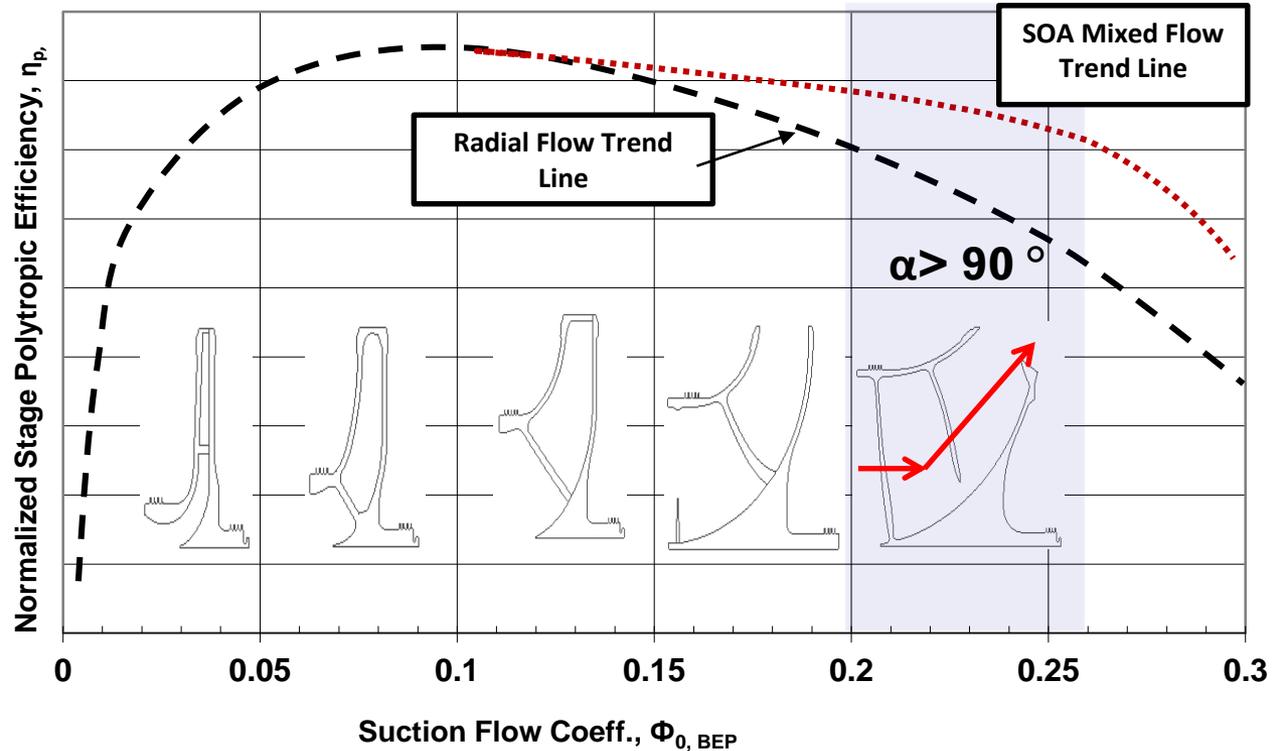
Characteristics:

Exit flow angle  $\alpha=90^\circ$

Peak Efficient  $\sim \Phi= 0.1$

Practical Limits  $\sim \Phi= 0.2$

# Mixed Flow Centrifugal stage



Characteristics:

Exit flow angle  $\alpha > 90^\circ$

Maintains Efficiency above radial well beyond 0.25

Practical Limits  $\sim \Phi = 0.3$

# State of the Art

## Second Generation Mixed Flow Stage

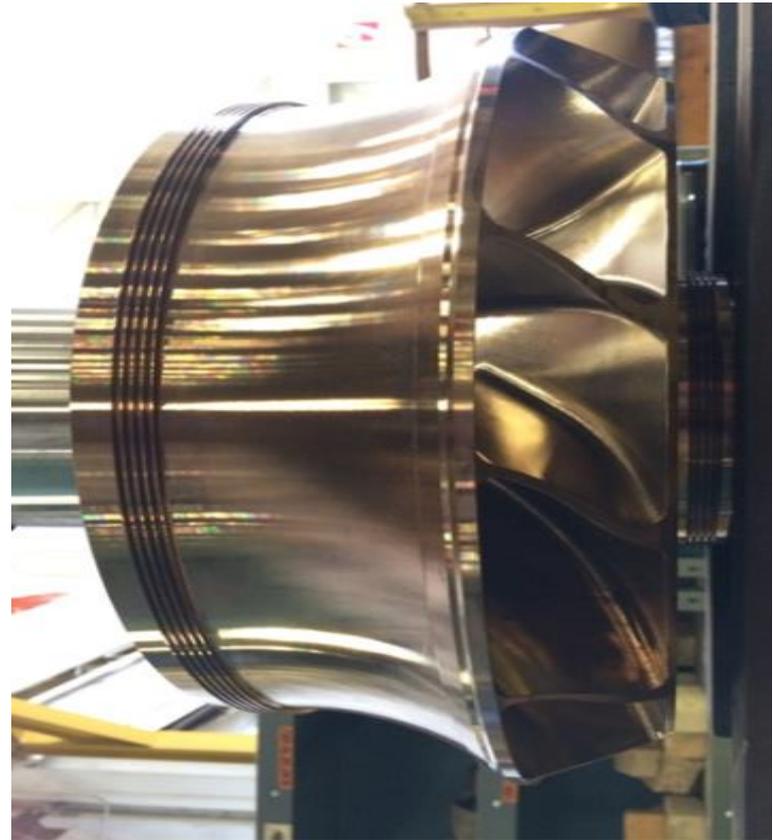


Optimum flow path sizing and aerodynamic throat area control using splitters.

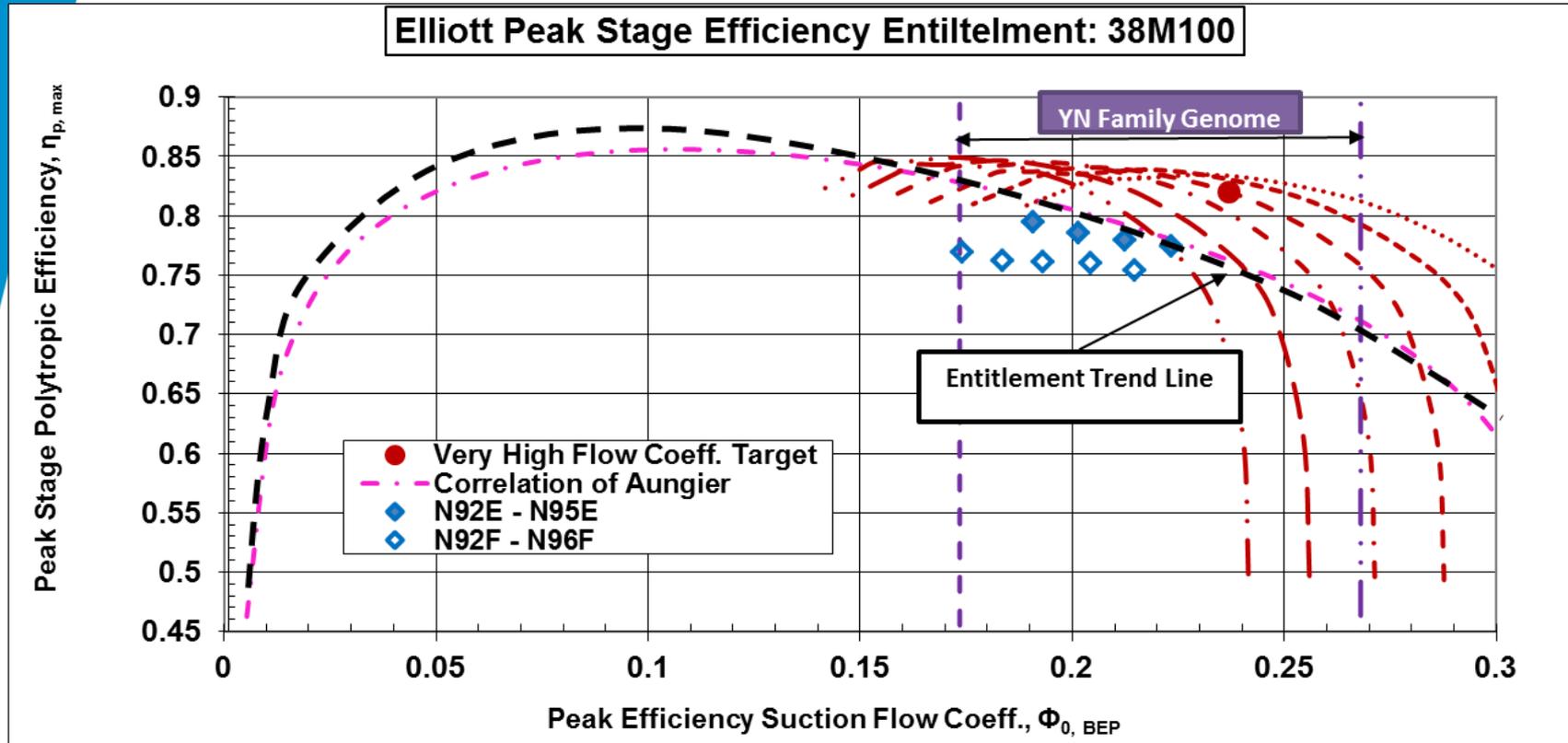
**First Generation Mixed Flow Stage**



# State of the Art Second Generation Mixed Flow Stage



# Built and Tested

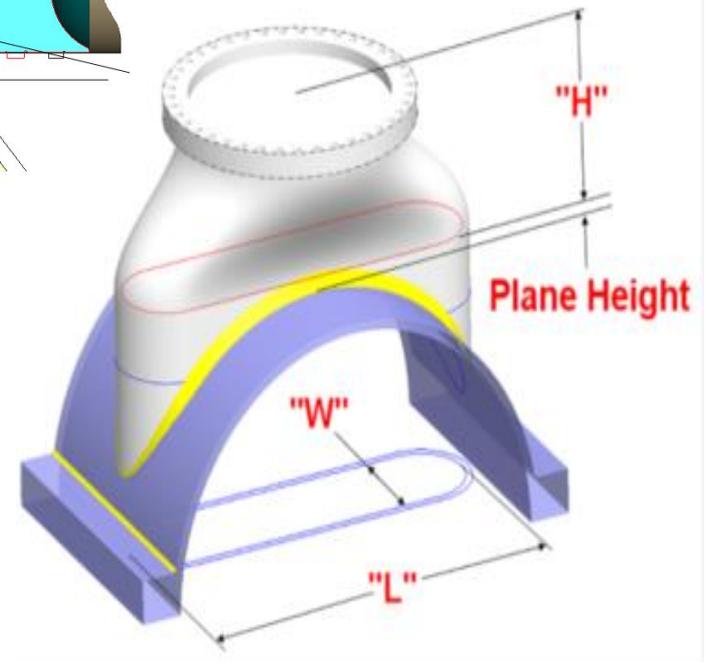
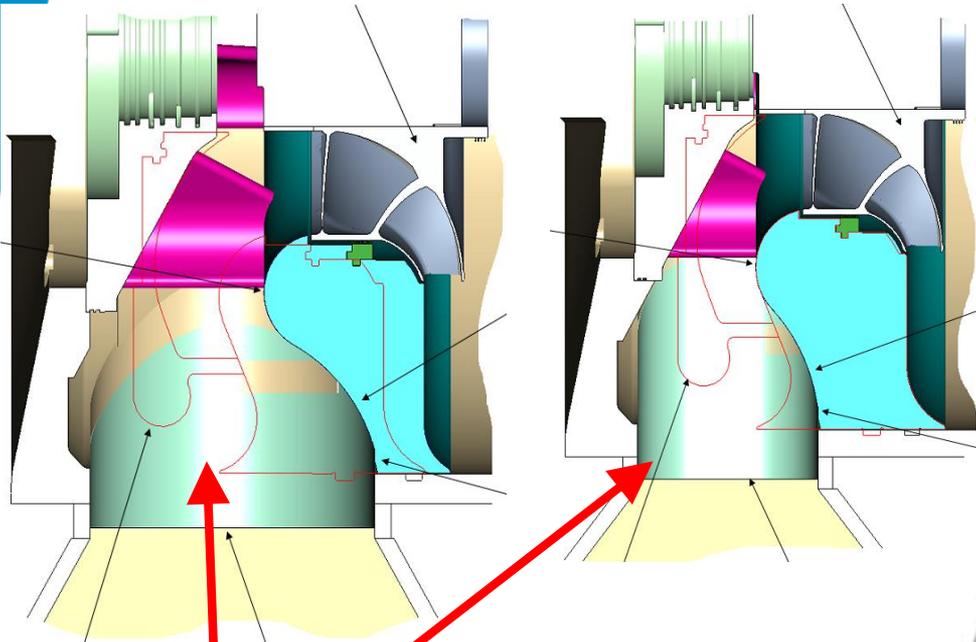


# Increased nozzle sizes

Larger nozzle sizes across all frame sizes  
Increases the flow capacity of the frame while  
improving bearing span

<b>Frame</b>	<b>Previous max inlet</b>	<b>Revised max inlet size</b>	<b>Previous max dsch</b>	<b>Revised max dsch size</b>
	inches	inches	inches	inches
<b>56</b>	<b>36</b>	<b>42</b>	<b>24</b>	<b>30</b>
<b>60</b>	<b>42</b>	<b>48</b>	<b>36</b>	<b>36</b>
<b>70</b>	<b>48</b>	<b>60</b>	<b>30</b>	<b>36</b>
<b>78</b>	<b>54</b>	<b>66</b>	<b>36</b>	<b>42</b>
<b>88</b>	<b>66</b>	<b>78</b>	<b>42</b>	<b>48</b>
<b>103</b>	<b>72</b>	<b>90</b>	<b>54</b>	<b>60</b>
<b>110</b>	<b>84</b>	<b>102</b>	<b>54</b>	<b>66</b>

# High Flow Axial Compact Nozzles



Similitude of Required Aeropath  
Preserved

# Case Study of a real 1500KTA plant

Comparison of: Sections 1,2 and 3 of the CGC

2011 design: Sec 1 88MD3-3 – Sec 2 88M4I

Compressor Rated Point: ~58MW @ ~3600rpm

88MD3-3 Sec1: 2x66" Inlets, 66" Discharge

88M4I Sec2/3: 60"/42" Inlets, 42"/36" Discharge

# High Flow Coefficient Selection

78MD3-3 – 78M4I

Compressor Rated Point: 58MW @ **4300**rpm

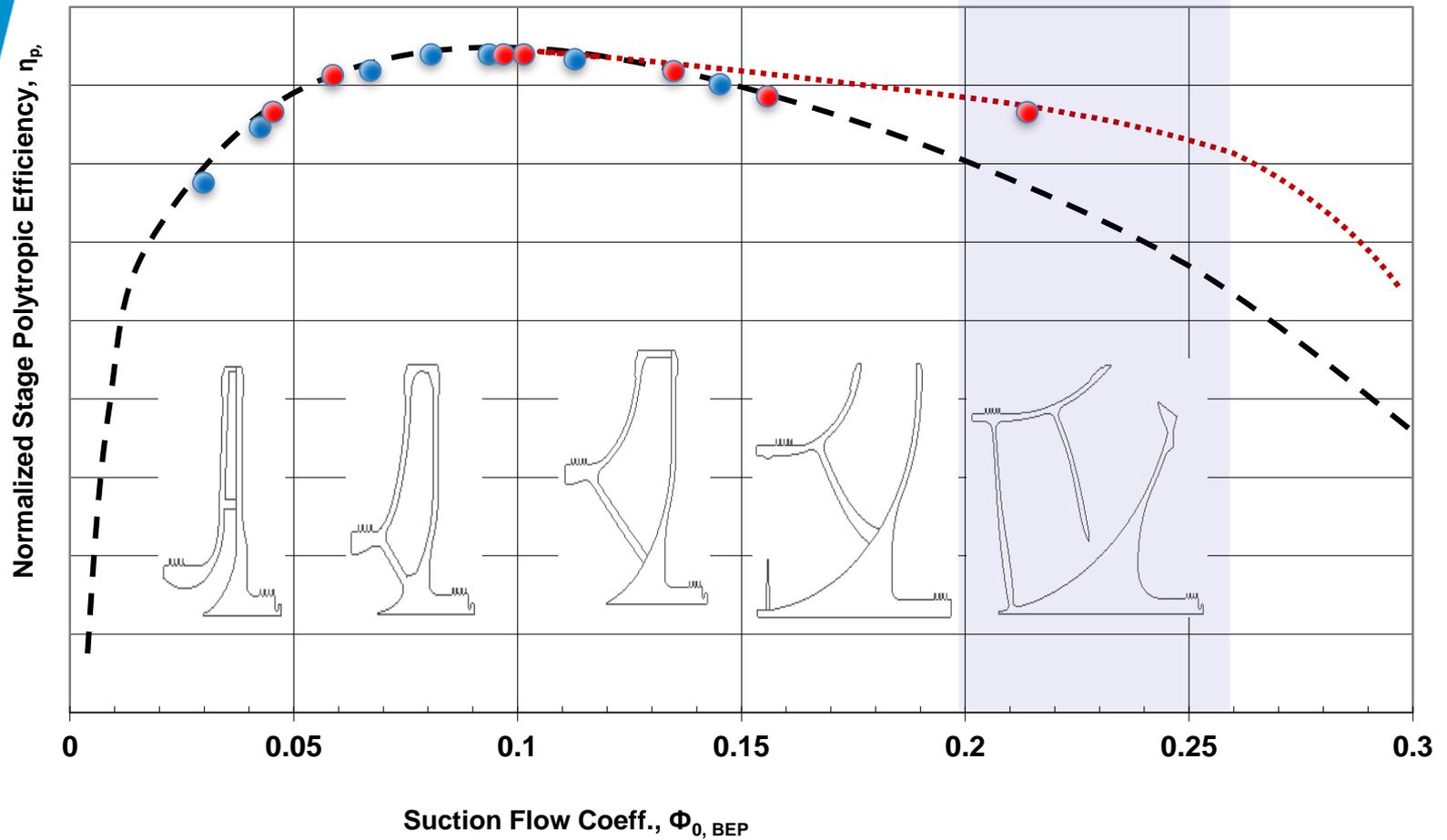
78MD3-3 Sec1: 2 x 66" Inlets, 66" Discharge

78M4I Sec2/3: 60"/42" Inlets 42"/36" Discharge

# Smaller Frames:

Casing	First Stage Flow Co $\Phi$	Bearing Span (m)	Rotor Weight (kg)	Unit Weight (kg)
88MD3-3	0.146	5.4	12,000	188,000
78MD3-3	0.214	4.8	9,000	145,000
Delta:	<b>+46.5%</b>	<b>-12%</b>	<b>-25%</b>	<b>-43,000</b> <b>-23%</b>
88M4I	0.0915 & 0.0431	4.4	11,500	168,000
78M4I	0.1351 & 0.0593	4.2	8,600	125,000
Delta:	<b>+48% &amp; +35%</b>	<b>-5%</b>	<b>-25%</b>	<b>-43,000</b> <b>-26%</b>

# Overall Compressor Efficiently impact



# The Future

The application of high flow coefficient staging is already being done.

This is not limited to 2000+ KTA plants. But also reducing the cost, weight and footprint of plants or all sizes.

Owners, operators, process licensors, EPCs and the equipment OEM need to work together to meet the challenges of the future.

# Questions?